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## О журнале

Международный научный периодический журнал "Научный взгляд в будущее" получил большое признание среди отечественных и зарубежных интеллектуалов. Сегодня в журнале публикуются авторы из России, Украины, Молдовы, Казахстана, Беларуси, Чехии, Болгарии, Литвы Польши и других государств.

Учрежден в 2015 году. Периодичность выхода: ежеквартально.

Основными целями журнала "Научный взгляд в будущее" являются:

- содействие обмену знаниями в научном сообществе;
- помочь молодым ученым в информировании научной общественности об их научных достижениях;
- создание основы для инноваций и новых научных подходов, а также открытый в неизвестных областях;
- содействие объединению профессиональных научных сил и формирование нового поколения ученых-специалистов в разных сферах.

Журнал целенаправленно знакомит читателя с оригинальными исследованиями авторов в различных областях науки, лучшими образцами научной публистики.

Публикации журнала "Научный взгляд в будущее" предназначены для широкой читательской аудитории – всех тех, кто любит науку. Материалы, публикуемые в журнале, отражают актуальные проблемы и затрагивают интересы всей общественности.

Каждая статья журнала включает обобщающую информацию на английском языке.

Журнал зарегистрирован в РИНЦ SCIENCE INDEX и INDEXCOPERNICUS.

## Про журнал

Міжнародний науковий періодичний журнал "Науковий погляд у майбутнє" отримав велике визнання серед вітчизняних і зарубіжних інтелектуалів. Сьогодні в журналі публікуються автори з Росії, України, Молдови, Казахстану, Білорусі, Чехії, Болгарії, Литви, Польщі та інших держав.

Дата заснування в 2015 році. Періодичність виходу: щоквартально

Основними цілями журналу є:

- сприяння обміну знаннями в науковому співтоваристві;
- допомога молодим вченим в інформуванні наукової громадськості про їх наукові досягнення;
- створення основи для інновацій і нових наукових підходів, а також відкриттів в невідомих областях;
- сприяння об'єднанню фахових наукових сил і формування нового покоління вчених-фахівців в різних сферах.

Журнал цілеспрямовано знайомить читача з оригінальними дослідженнями авторів в різних областях науки, кращими зразками наукової публістики.

Публікації журналу призначенні для широкої читацької аудиторії - усіх тих, хто любить науку. Матеріали, що публікуються в журналі, відображають актуальні проблеми і зачіпають інтереси всієї громадськості.

Кожна стаття журналу включає узагальнючу інформацію англійською мовою.

Журнал зареєстрований в РИНЦ SCIENCE INDEX і INDEXCOPERNICUS.

## About the journal

The International Scientific Periodical Journal "*Scientific look into the future*" has gained considerable recognition among domestic and foreign researchers and scholars. Today, the journal publishes authors from Russia, Ukraine, Moldova, Kazakhstan, Belarus, Czech Republic, Bulgaria, Lithuania, Poland and other countries.

Journal Established in 2015. Periodicity of publication: Quarterly

The journal activity is driven by the following objectives:

- Broadcasting young researchers and scholars outcomes to wide scientific audience
- Fostering knowledge exchange in scientific community
- Promotion of the unification in scientific approach
- Creation of basis for innovation and new scientific approaches as well as discoveries in unknown domains

The journal purposefully acquaints the reader with the original research of authors in various fields of science, the best examples of scientific journalism.

Publications of the journal are intended for a wide readership - all those who love science. The materials published in the journal reflect current problems and affect the interests of the entire public.

Each article in the journal includes general information in English.

The journal is registered in the RISC SCIENCE INDEX and INDEXCOPERNICUS.





## Положение об этике публикации научных данных и ее нарушениях

Редакция журнала осознает тот факт, что в академическом сообществе достаточно широко распространены случаи нарушения этики публикации научных исследований. В качестве наиболее заметных и вопиющих можно выделить плагиат, направление в журнал ранее опубликованных материалов, незаконное присвоение результатов чужих научных исследований, а также фальсификацию данных. Мы выступаем против подобных практик.

Редакция убеждена в том, что нарушения авторских прав и моральных норм не только неприемлемы с этической точки зрения, но и служат препятствием на пути развития научного знания. Потому мы полагаем, что борьба с этими явлениями должна стать целью и результатом совместных усилий наших авторов, редакторов, рецензентов, читателей и всего академического сообщества. Мы призываем всех заинтересованных лиц сотрудничать и участвовать в обмене информацией в целях борьбы с нарушением этики публикации научных исследований.

Со своей стороны редакция готова приложить все усилия к выявлению и пресечению подобных неприемлемых практик. Мы обещаем принимать соответствующие меры, а также обращать пристальное внимание на любую предоставленную нам информацию, которая будет свидетельствовать о неэтичном поведении того или иного автора.

Обнаружение нарушений этики влечет за собой отказ в публикации. Если будет выявлено, что статья содержит откровенную клевету, нарушает законодательство или нормы авторского права, то редакция считает себя обязанной удалить ее с веб-ресурса и из баз цитирования. Подобные крайние меры могут быть применены исключительно при соблюдении максимальной открытости и публичности.

## Положення про етику публікації наукових даних і її порушеннях

Редакція журналу усвідомлює той факт, що в академічній спільноті досить широко поширені випадки порушення етики публікації наукових досліджень. В якості найбільш помітних можна виділити плагіат, відправлення в журнал раніше опублікованих матеріалів, незаконне привласнення результатів чужих наукових досліджень, а також фальсифікацію даних. Ми виступаємо проти подібних практик.

Редакція переконана в тому, що порушення авторських прав і моральних норм не тільки неприйнятні з етичної точки зору, але і служать перешкодою на шляху розвитку наукового знання. Тому ми вважаємо, що боротьба з цими явищами повинна стати метою і результатом спільних зусиль наших авторів, редакторів, рецензентів, читачів і усієї академічної спільноти. Ми закликаємо всіх зацікавлених осіб співпрацювати і брати участь в обміні інформацією з метою боротьби з порушенням етики публікації наукових досліджень.

Зі свого боку редакція готова докласти всіх зусиль до виявлення та припинення подібних неприйнятніх практик. Ми обіцяємо вживати відповідних заходів, а також звертати пильну увагу на будь-яку надану нам інформацію, яка буде свідчити про неетичну поведінку того чи іншого автора.

Виявлення порушень етики тягне за собою відмову в публікації. Якщо буде виявлено, що стаття містить відвертий наклеп, порушує законодавство або норми авторського права, то редакція вважає себе зобов'язаною видалити її з веб-ресурсу і з баз цитування. Подібні крайні заходи можуть бути застосовані виключно при дотриманні максимальної відкритості і публічності.

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The editors of the journal are aware of the fact that in the academic community there are quite widespread cases of violation of the ethics of the publication of scientific research. As the most notable and egregious, one can single out plagiarism, the posting of previously published materials, the misappropriation of the results of foreign scientific research, and falsification of data. We oppose such practices.

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УДК 622.245.52

**EXPERIMENTAL RESEARCH OF HYDRODYNAMIC PULSATATOR  
OPERATION AND ITS INFLUENCE ON OIL PARAMETERS**  
**ЕКСПЕРИМЕНТАЛЬНІ ДОСЛІДЖЕННЯ РОБОТИ ГІДРОДИНАМІЧНОГО  
ПУЛЬСАТОРА ТА ЙОГО ВПЛИВ НА ПАРАМЕТРИ НАФТИ**

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**Abstract.** The article presents the experimental studies of the hydrodynamic pulsator operation and intensity determination of the ultrasonic field produced by the device, as well as its effect on the high-viscosity oil parameters of the Kokhanivske deposit.

The paper also described the improved design of the hydrodynamic pulsator, which is used in the technological scheme when extracting high-viscosity oils from wells onto the surface.

**Key words:** oil, pulsator, vibration, ultrasound, intensity, viscosity, temperature.

### Introduction.

Geological resources of high-viscosity oils and natural bitumen exceed the resources of conventional oil. 75% of high-viscosity oils are at the depths of up to 2,000 m. The main complications while operating the layers that contain high-viscosity oil (HVO) are related to the oil physical and chemical properties. The increase in viscosity and decrease in temperature when extracting oil onto the surface, as well as the significant content of asphaltene-osmyl-paraffinic substances, lead to substantial pressure losses in the bottomhole formation zone and wellbore, as well as to intensive deposition of dense hydrocarbons on oil-well tubing and, as a result, decrease in the wells production capabilities and increase in the total costs for the wells operation. The elimination of these shortcomings would increase production of high-viscosity oil in the Ukrainian fields. In order to do this, it is necessary to solve a number of problems that have not been resolved yet.

One of such problems is the improvement in the production methods and pumping equipment for high-viscosity oil extraction, the solution of which is very relevant at the present stage of oil extraction. There is an intensive search for new technologies and technical means based on new physical phenomena and effects in all countries today, in particular, creation and study of the pulsation devices operation, as well as determination of the hydrodynamic vibration effect on the decrease of oil viscosity.

### Analysis of Literary Data and Formulation of the Problem.

In Ukraine, the extraction of high-viscosity oil is carried out by means of borehole method. The works of such scientists as I. M. Mishchenko and O. F. Myronov [1] state that one of the most suitable means for extraction of HVO are jet pumps. These pumps have no moving parts and when provided in the plug-in



version they can be replaced without being lifted onto the surface of the tubing. The only problem for jet pumps is the HVO intake.

One of the ways to reduce the negative effect of high-viscosity oil on its intake to the inlet line of the pump is to combine the operation of jet pump with the pulsating effect on high-viscosity oil. This will positively affect the operation of the pump when operating the formation that contains HVO at the depths of up to 2,000 m.

Taking into account the results of the bench tests [2], it was concluded that it is better to use the hydrodynamic pulsator as a generator of pulsation vibrations. Such devices have small dimensions and weight, as well as simple design that does not contain any moving parts, their flow part is not vulnerable to cavitation fracture, and they are easily mounted in any jet apparatus.

When designing the hydrodynamic pulsator, the analysis of similar domestic and foreign devices (such as the Hartmaniv type generator, vortex generators, hydroacoustic emitters with resonating rods (plate, membrane), devices designed on the basis of the Venturi tube, etc.) was carried out.

We considered hydroacoustic generators [3], whose operation principle is based on the flow direction change or interaction of two or more twisted jets. Generation of vibrations is determined when the rotating flow is disrupted from the section of the exit cone, as well as by the instability of the rotating jet and deformation of the peripheral flow with periodic pulsation. The liquid jet is fed through the tangentially located hole (or several holes), starts rotating in the vortex chamber, coming out of it through the narrowed outlet hole, increases the rotational motion, and breaks off the sharp edge of the outlet hole. In this case, pulsations of the output flow occur. They are intensified by the jet (whose value can be adjusted) supplied through the central hole. If the central jet is shifted with the eccentricity of 0.5-1.5 mm, the development of the self-oscillating process intensifies, the amplitude of the near-axial flow precession increases, the level of the pressure and velocity pulsation in the peripheral vortex rises, and, accordingly, the power of the emitted field and generator efficiency factor increases.

The emergence of chemical reactions in the field of ultrasonic waves is closely related to the cavitation phenomenon, which contributes to formation of cavities in the liquid, followed by their burst and accompanied by intense hydraulic shocks. The cavity pocket is formed inside the liquid, provided that the pressure is reduced to the value that is less than the ultimate strength of this liquid [4-6].

The vortex-type hydrodynamic radiator [7], in which rotating fluid flows in opposite directions were created, was also considered. The cylindrical body and devices for creating rotating fluid flows (made in the form of cylindrical coaxially arranged elements that create annular gaps at the outlet) were used for this purpose (and helical channels were also made at the inlet). These helical channels are made on complex cylindrical elements and have an opposite direction. The cylindrical elements are also of conical shape. Such devices were tested in laboratory conditions and although good results have been obtained, it is necessary to further research and try to use them in practice.



## Purpose and Objectives of the Study.

The purpose of the study is to determine the intensity of the generating field created by the hydrodynamic pulsator and its effect on reducing the viscosity and increasing the temperature of high-viscosity oils.

The tasks resolved to achieve this aim included the following:

- having analyzed positive and negative aspects of the existing generators, to create an improved design of the hydrodynamic pulsator, which would create a big field intensity;
- to develop a scheme and make a bench for carrying out experimental studies of the improved design of the hydrodynamic pulsator.

## Materials and Methods for Studying the Hydrodynamic Pulsator Operation.

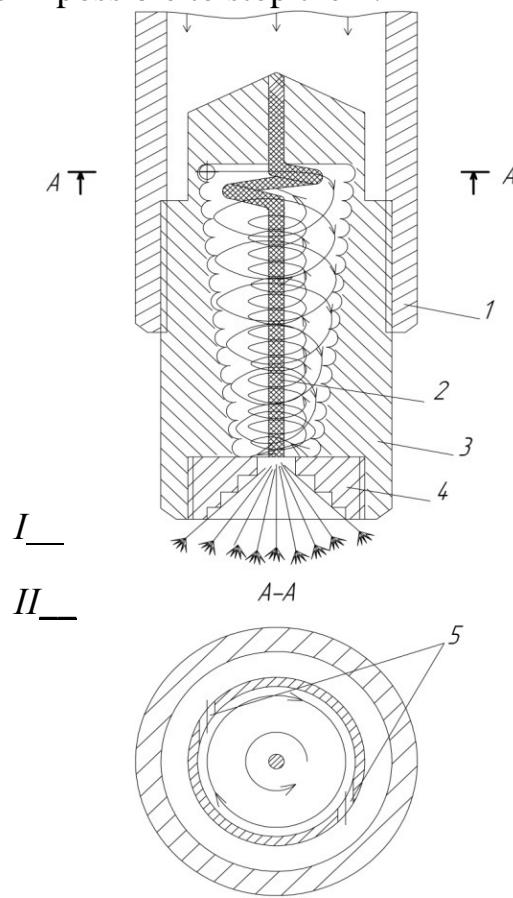
In order to improve the design of the hydrodynamic pulsator, we use a cone-shaped vortex chamber with tangential channels, as well as with the inner surface of the body, made in the form of a helical surface for greater whirling of the liquid flow. A diffuser with stepped sharp edges and expansion angle of more than  $30^0$  (Fig. 1) was proposed to increase the intensity of the generating field and formation of periodically stalling cavitation with rapid collapse of the cavitation caverns.

To reduce the flow rate of the working fluid, it is necessary to decrease the nozzle diameter of the critical part. Since this value is limiting and depends on cleaning of working fluid (the filters with the diameter of no more than 2.5 mm are used), the nozzle diameter can be taken not less than 3 mm, because the nozzle can become clogged with sand, scale, and similar cuttings, which will slip through the filter. Therefore, it has been proposed to use the diffuser with the nozzle diameter of the critical part of more than 3 mm, as well as the spring core of smaller diameter than the nozzle diameter, which will create an annular gap with the cross-sectional area that is approximately equal to the critical one. The availability of the spring core initiates formation of the helical vortex cord, which when rotating around the core, deforms the peripheral flow, causing periodic pulsations of velocity and pressure in it that results in an increase of the intensity of the generating field.

The working fluid flows through the nozzle 1 into the inlet tangential holes 5 and into the annular cone-shaped vortex chamber 3, where the liquid flow is strongly spun under the influence of the centrifugal force and initiates emergence of a precession vortex core that is swirled along the jet length. When moving along the walls of the circular cone-shaped chamber from the cross-section with larger diameter to the cross-section with smaller diameter, the swirling flow increases its speed. The increase in the flow rate means an increase in the kinetic energy of the jet. According to the law of energy conservation, the growth of kinetic energy will inevitably cause a drop in potential energy and the role of the potential energy in the flow of the working fluid is performed by pressure. Thus, the smaller the diameter, the higher the speed of the swirling jet in it and the lower the pressure drop. As soon as the pressure drop value approaches the value of the saturated vapor pressure, a rapid evaporation will begin, i. e., the cold adiabatic boiling of the liquid will start. This process will be accompanied by formation of bubbles, inside of which there will be the liquid vapor. The lower end of the central spring core 2, when being under the simultaneous action



of the differentials of the swirling jet speed and precession vortex core, will make transverse vibrational movements, creating an even greater vortex and intensifying formation of vapor-and-gas bubbles or caverns. When the liquid passes through the step diffuser 4, the diameter of which will gradually increase, the fluid velocity will decrease and the pressure will rise at the exit of the vortex chamber. The walls of the vapor bubbles, the inner pressure of which will be below atmospheric pressure, will begin moving rapidly towards each other. The greater the external pressure, the greater the force acting on the walls and the greater their acceleration. Some insignificant portion of the vapor will always be present in the bubble volume. Its amount is small and, therefore, the vapor does not exercise any significant resistance to the convergence of the bubble walls during the most part of the burst process. And it is only at the end, when the bubble volume is a percentage or a fraction of a percent of its maximum volume, their pressure value approaches the value of the external pressure exerted on the bubble walls. However, since the walls have already gained some speed and inertia, it is impossible to stop them.



(Author's development)

**Fig. 1. Scheme of hydrodynamic pulsator:** 1 – branch pipe; 2 – spring core; 3 – cone-shaped vortex chamber; 4 – step diffuser; 5 – tangential input channels; I, II – nozzle cross-section

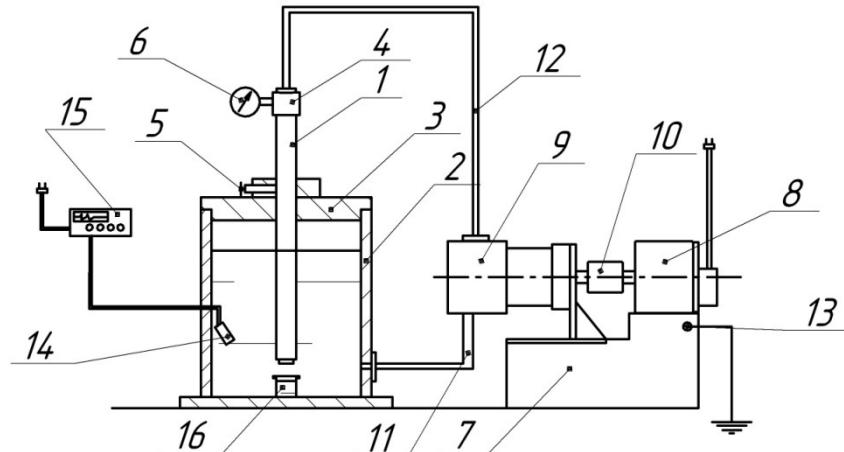
As a result, the velocity pressure of the walls continues compressing the bubble so it bursts and powerful microflows like cumulative jets appear. At this moment, the liquid will be heated by the energy released when the jet brakes during the cavitation processes, i. e. due to hydraulic friction.



At the same time, the increase in the pressure will lead to the reverse process – vapor condensation. The temperature in the center of the burst bubble will greatly exceed the temperature of the working fluid as a result of compression. This excess, according to some scientists, can reach tens or even hundreds of degrees.

In order to carry out the study, the bench, consisting of the following main parts, was designed: power module, hydrodynamic pulsator, chamber where physical fields would be studied, primary sensors, and secondary measuring equipment necessary for determining the parameters of the physical fields.

The power module of the bench is equipped with the pump whose flow rate through the nozzle with the cross-sectional area of approximately  $7.5 \cdot 10^{-6} \text{ m}^2$  is, on average,  $0.2 \cdot 10^{-3} \text{ m}^3/\text{s}$  at the pressure of 10 MPa. This could be a plunger, vane, rotary or gear pump. Furthermore, there is a need for an electric motor with the power of up to 3 kW and number of revolutions equal to about  $50 \text{ s}^{-1}$  (3000 rpm). The electric motor and pump should be mounted on a common frame and connected with each other by couplings. There also should be some grounding. The scheme of the laboratory bench is shown in Fig. 2 and 3.



(Author's development)

**Fig. 2. Scheme of the laboratory bench for determining the intensity of the energy field produced by the hydrodynamic pulsator:** 1 – hydrodynamic pulsator; 2 – metal chamber; 3 – chamber cover; 4 – adapter; 5 – stop screw; 6 – manometer; 7 – frame; 8 – electric motor; 9 – piston pump; 10 – coupling; 11 – suction line; 12 – discharge line; 13 – ground terminal; 14 – magnetostriuctive sensor; 15 – oscilloscope; 16 – capsule with high viscosity oil

The hydraulic part of the bench was made with the closed cycle, for example, the working fluid from the technical tank goes through the suction line into the pump and gets to the discharge line, from where it is fed through the flowmeter and filter into the hydrodynamic pulsator, which is located in the study chamber filled with liquid, wherefrom the discharge liquid returns to the technical tank.

It is necessary to calculate the maximum permissible pressure for the chamber (technical tank), in which the pulsator operates, by the following formula:

$$P_{\max} = k_i P_e, \quad (1)$$

where  $k_i = 1,5$  – reliability factor;



$P_{\hat{e}}$  – pressure inside the chamber, Pa.

Stresses arising in the chamber,  $\sigma_k$  are determined by the formula of annular radial and axial stresses:

$$\sigma_k = \sigma_o = \frac{P_{\max} D_{\hat{a}}}{2\delta} \leq [\sigma_{\delta}], \quad (2)$$

where  $D_{\hat{a}}$  – inner chamber diameter, m;

$\delta$  – chamber wall diameter, m;

$[\sigma_{\delta}]$  – permissible tensile stresses for chamber material, Pa.



**Fig. 3. Photo of the laboratory bench for studying the hydrodynamic pulsator operation**

The studies with the help of the laboratory bench were carried out in two stages. The first stage was the choice of the optimum pulsator operation modes and determination of the parameters of the energy field produced by the hydrodynamic pulsator under various initial conditions, i. e. at a given pressure and flow rate at the hydrodynamic pulsator inlet. The second stage was the study of the influence of the energy fields created by the hydrodynamic pulsator on the decrease in viscosity and increase in temperature of the asphaltene-tar-paraffinic oil when the pulsator operates in optimal modes.

In order to define the synergistic effect of the energy field created by the hydrodynamic pulsator, it is necessary to separately determine the effect of the energy field and then – the effect of the thermal field and phenomenon of cavitation. For these purposes, it is necessary to have primary sensors (measuring transducers) – the devices that perceive a measured parameter and convert it into an output signal (usually electric), which is convenient for transmission via communication lines to secondary devices for further conversion, recording, and processing in order to obtain a result in the form of a measured physical quantity as a function of time.

The intensity of the ultrasonic field can be calculated according to the following formula



$$I = 2\pi \cdot A_0^2 f^2 \rho \cdot c, \quad (3)$$

where  $A_0$  – displacement amplitude, m;  
 $f$  – oscillation frequency,  $\text{s}^{-1}$ ;  
 $\rho$  – environment density,  $\text{kg/m}^3$ ;  
 $c$  – speed of sound in this environment, m/s.

The density of the environment and speed of sound in it can be taken as tabular or calculated from known formulas.

Furthermore, the intensity of the field created by the hydrodynamic pulsator can be determined through multiplication of the side quantities, using the following formula

$$I = \frac{PQ}{S}, \quad (4)$$

where  $P$  – pressure inside the nozzle, Pa;  
 $Q$  – liquid flow rate through the nozzle,  $\text{m}^3/\text{s}$ ;  
 $S$  – area of the nozzle cross-section,  $\text{m}^2$ .

Therefore, in order to measure these values, it is necessary to have a flowmeter and manometers or pressure gauges on the bench.

When comparing the results obtained with the help of formulas 3 and 4, it is possible to state with greater certainty about the intensity of the energy field produced by the hydrodynamic pulsator, as well as it is easier to determine optimal modes of its operation.

In order to determine the thermal field, it is necessary to measure the difference in temperatures at the inlet and outlet of the hydrodynamic pulsator. For this purpose, glass liquid thermometers (alcohol or mercury), electric contact thermometers of TPK type with a movable contact, and thermoelectric converters or as they are also called thermocouples of the TMK (copper-copel) or TKhK (chrome-copes) types can be used. However, when determining these parameters, it is necessary to take into account the time and volume of the liquid heated over a given period of time.

The speed of ultrasound propagation in the material environment is determined by its characteristics, such as elasticity and density. However, when there is an increase in some ultrasonic intensity that is limiting for a given environment and when the propagation of the small amplitude oscillations changes into the propagation of the finite amplitude oscillations, nonlinear effects begin to play an increasing role in the field of ultrasonic oscillations. Violation of the principle of the wave process superposition leads to emergence of new physical phenomena – radiation pressure, acoustic fluxes, and acoustic cavitation, which is the most important manifestation of the action of powerful ultrasound on the liquid.

Vapor-gas bubbles, which nonlinearly pulsate, burst, and format shock waves and cumulative jets, emerge and grow in the liquid during cavitation. The propagation of the powerful finite amplitude ultrasound in the liquid with the



development of cavitation phenomena is accompanied by a series of physicochemical processes that are of great practical significance – degassing, emulsification, coagulation, dispersion, etc.

Since it is already known that the cavitation formation depends on the viscosity of the fluid, in which the oscillations propagate, it would be desirable to conduct the studies using a light and low-viscosity oil as the working fluid, because light oil is used as a solvent for extraction of high-viscosity oils. Moreover, having studied the action of the hydrodynamic pulsator, in which low-viscosity oil is used as a working fluid in optimal operating modes, it is possible to achieve a significant reduction in the viscosity of heavy asphaltene-tar-paraffinic oils.

The studies were carried out with the help of the laboratory bench, consisting of the metal chamber (technical tank) for studying physical fields created with the help of the hydrodynamic pulsator; the hydraulic part of the bench was made with a closed cycle – the working fluid was supplied from the technical tank through the pump to the hydrodynamic pulsator and into the metal chamber, wherefrom it returned to the technical tank through the discharge line. In order to measure the temperature, glass alcohol thermometers were used and high-viscosity oil from the Kokhanivske field was used as a studied oil.

In order to determine the pressure in the nozzle, the Bernoulli equation [8] was used for two cross-sections 1 and 2, made in a steady flow of a real liquid

$$P_1 + \alpha_1 \frac{\rho \cdot v_{cp1}^2}{2} + \rho \cdot g \cdot z_1 = P_2 + \alpha_2 \frac{\rho \cdot v_{cp2}^2}{2} + \rho g z_2 + \Delta p_{12}, \quad (5)$$

where  $P$  – static pressure, Pa;

$v_{\text{ср}}$  – average velocity in this cross-section, equal to the ratio of the second volume flow rate to the cross-sectional area, m/s;

$\rho$  – working fluid density, kg/m<sup>3</sup>;

$z$  – jet cross-section height above the arbitrary level, m;

$\alpha_1$  – correction factor for the nonuniformity of the velocity propagation across cross-sections 1 and 2;

$\Delta p_{12}$  – loss of pressure between cross-sections 1 and 2, associated with the work of frictional forces.

## Results of the Studies of the Intensity of the Ultrasonic Field Produced by the Hydrodynamic Pulsator

A number of experiments were performed with the help of the laboratory bench to determine the intensity of the ultrasonic field (Fig. 2). The results of the tests are summarized in Table 1.

The high-viscosity oil from the Kokhanivske field was placed into a container and then subjected to the action of the hydroacoustic field created by the pulsator. As a result, the oil viscosity decreased from 147 mPa·s to 18 mPa·s. At the same time, the temperature of the treated oil increased from 15°C to 58°C in half an hour.



Table 1

**Results of the laboratory studies of the intensity of the ultrasonic field produced by the hydrodynamic pulsator**

Nozzle cross-section area, $\text{m}^2 \cdot 10^{-6}$	Pressure inside the discharge line, $\text{Pa} \cdot 10^6$	Volume of the liquid from the pulsator nozzle, $\text{m}^3 \cdot 10^{-3}$	Time, during which the given volume of liquid flows out, s	Intensity of the ultrasonic field, $\text{W/m}^2 \cdot 10^3$
7.06	0.118	0.62	9	1.153
		0.67	10	1.120
		0.74	11	1.121
		0.69	10	1.153
		0.68	10	1.136
7.06	2.06	1.3	7	54.18
		1.6	9	51.64
		1.28	6	62.45
		1.38	7	57.49
4.15	6.81	0.86	6	234.26
		0.99	6	270.36
		0.96	6	262.87
		0.98	6	266.95

(Author's development)

The intensity of the ultrasonic field is determined with the help of [8] by the following formula

$$I = P \cdot v, \quad (6)$$

where  $P$  – pressure inside the discharge line, Pa;

$v$  – velocity of the liquid flowing from the nozzle, m/s;

$$v = \frac{Q}{S}, \quad (7)$$

where  $Q$  – flow rate of the liquid through the pulsator nozzle,  $\text{m}^3/\text{s}$ ;

$S$  – area of the nozzle cross-section,  $\text{m}^2$ ;

$$Q = \frac{V}{t}, \quad (8)$$

where  $V$  – volume of the liquid flowing from the cavitator nozzle,  $\text{m}^3$ ;

$t$  – time, during which the given volume of fluid flows out, s.

**Discussion of the Results of the Laboratory Studies of the Intensity of the Ultrasonic Field Produced by the Hydrodynamic Pulsator**

The laboratory studies of the hydrodynamic pulsator determined the nature of the working fluid flowing from the device. The jet, getting through the tangential holes into the vortex chamber, acquires some centrifugal acceleration and creates a hydroacoustic field when flowing out at a high speed through the pulsator nozzle [9].



The optimum mode of the hydrodynamic pulsator operation (see Table 1) occurs at the nozzle cross-section area of  $4.15 \text{ m}^2 \cdot 10^{-6}$ , pressure in the discharge line of 6.81 MPa, and ultrasonic field intensity of  $234.26\text{--}266.95 \text{ W/m}^2 \cdot 10^3$ , i. e. when the diameter of the nozzle is smaller, the value of the field intensity created is larger.

The viscosity of the Kokhanivske field oil decreased to 18 mPa·s (at the end of the studies) after treatment with the help of the hydroacoustic field when compared with the original value of 147 mPa·s.

At the same time, the temperature of the oil increased during the experiment: the initial value was 15°C and it grew to 58°C at the end of the studies. This indicates that some part of the energy of the hydroacoustic field is transformed into heat. During the operation of the hydrodynamic pulsator, transient pressure gradients arise, the mechanical structure of the high-viscosity oil is destroyed, and the non-Newtonian liquid is transformed into a Newtonian one, which is confirmed by the results of the experiments provided in [10-17].

## Conclusions

Based on the experimental studies carried out, it was established that pulsations and pressure oscillations can arise in the flow of the working fluid as it passes through the hydrodynamic pulsator.

Using the designed and manufactured bench, it became possible to determine the intensity of the hydroacoustic field, the value of which is sufficient to reduce the viscosity of the high-viscosity oil (from 147 mPa·s to 18 mPa·s), which allows to take oil into the intake line of the jet pumps without any difficulties.

The most significant effect of the hydrodynamic pulsator operation is the transition of the non-Newtonian oil into the Newtonian one due to destruction of the oil mechanical structure, which leads to an increase in the oil temperature.

The combination of these factors makes it possible to use the hydrodynamic pulsator in the technological scheme for extracting high-viscosity oils from wells onto the surface by increasing the flow rate of the high-viscosity oil pumping-out.

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*У статті описана вдосконалена конструкція гідродинамічного пульсатора, який застосовується в технологічній схемі при підніманні високов'язких нафт з свердловин на денну поверхню. Також представлена схема проведення лабораторних досліджень гідродинамічного пульсатора. Отримані результати свідчать про те, що при роботі цього пристрою в нафті Коханівського родовища виникають фізичні поля - ультразвукове, теплове і кавітаційне, які сприяють зниженню в'язкості нафти і збільшенню її температури. Експериментально встановлено, що під дією акустичного поля (ультразвуку) виникають швидкоплинні градієнти тиску і відбувається руйнування прикордонних шарів рідини, перехід неньютонівської рідини в ньютонівську. При певній інтенсивності поля (більше 0,1 кВт/м<sup>2</sup>) більше 50 % акустичної енергії трансформується в тепло. Таким чином, нафта одночасно опромінюється тепловим (термоакустична дія) і акустичним (ультразвуковим) полями. У високоінтенсивному акустичному (ультразвуковому) полі виникають так звані гравітаційні ефекти, які призводять до випадання механічних домішок, твердого парафіну і солей.*

*Ключові слова:* нафта, пульсатор, коливання, ультразвук, інтенсивність, в'язкість, температура.

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